Mechanical Characteristics Testing of Biodegradable Ramie Fiber Reinforced Polylactic Acid (PLA) Fabricated with Hot-Press Molding

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Abstract. In this research, composite material was fabricated from both renewable resources and biodegradable materials: ramie woven fabric as reinforcement and 3D printed polylactic acid (PLA) filament as resin matrix. The laminate composites were produced using a film stacking method and processed using hot-press molding. The mechanical properties of woven ramie fabric, PLA matrix, and laminate composites were investigated. It is shown that the breaking force of the plain woven ramie fabric in the warp direction was greater than in the weft direction. Further, the tensile and impact properties of laminate at warp direction higher than weft direction when ramie fabric reinforcement is used. In addition, scanning electron microscopy examination of laminate composite showed good bonding between ramie fiber and PLA matrix. In summary, laminated composites based on polylactic acid and woven ramie fabric display good performance capability, which can use for the development of engineering applications.

Keywords: Biodegradable, mechanical characterization, PLA, ramie.

INTRODUCTION

Pollution caused by plastics has become one of the most pressing environmental problems, due to the large increase in the production of disposable plastic products as population growth. Countries in Asia and Africa have a very severe problem of plastic pollution, where the garbage collection system is still neglected. But the developed world, especially in countries with low recycling rates, still have problems regarding the collection of used plastic (Laura Parker 2019). For this reason, it is necessary to use biodegradable plastic materials to prevent or reduce pollution in the use of synthetic plastics. One of the biodegradable plastics that can be an alternative to synthetic plastics is polylactic acid (PLA). PLA is a biodegradable and biocompatible polymer that can be applied to various industries, especially in packaging and biomedical materials (Sengupta et al. 2018). By reinforcing PLA with some natural fibers, PLA is expected to replace synthetic plastic (Yusoff et al. 2016; Chin et al. 2017; Alias et al. 2018). The use of natural fibers as reinforcement is so that the composite material produced can be fully biodegradable so that it can be called biocomposite (Alias et al. 2018; Chaitanya et al. 2019; Komal et al. 2019).

Several studies have reported that PLA can be reinforced with several types of natural fibers, for example with kenaf (Yusoff et al. 2016; Alias et al. 2018, Hassan et al. 2018), ramie (Yu and Li 2014; Yu et al. 2014; Yu et al. 2015), jute (Aguilar et al. 2018; Rajesh et al. 2018; Jiang et al. 2019), and bamboo (Sukmawan et al. 2016; Sinha et al. 2018; Li et al. 2019).

From these natural fibers, ramie is a natural fiber that has mechanical properties, especially tensile is quite good and easy to obtain because it can be cultivated in Indonesia. Furthermore, ramie fiber will be used as reinforced in PLA matrix in this study.

Recently, PLA is an expensive and hard to get material in Indonesia. PLA available in the Indonesian market is PLA which is commonly used for 3D printing. For this reason, this research will use PLA material for 3D printing, and will see how its mechanical properties when reinforced with ramie fabric. In this article, it is presented the preparation and mechanical characterization of an environmental friendly composite material manufactured from woven ramie fabric and polylactic acid (PLA). The evaluation of mechanical properties of ramie fabric, PLA matrix and laminate were determined. The specimens were prepared and tested according to the ASTM standard.

MATERIALS AND METHODS

Study area
The PLA polymer used in this research was transparent 3D printer PLA filament CCTREE A8012 with the diameter of 1.75 mm from 3D Zaiku Indonesia with raw material was imported from Natureworks.

The plain woven ramie fabrics were manufactured in Majalaya Textile Production Center, Bandung, West Java Indonesia using ramie fiber yarns from Koperasi Pondok Pesantren Darussalam, Garut, West Java, Indonesia.

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**Procedures**

- **Composite preparation**
  The PLA filament was cut into PLA granulate using strand pelletizer CSG 171/1 Collin GmbH. The PLA plate was produced using hot-press molding with the mold temperature of 200°C and the pressure of 0.5 MPa.

  Composite panels (17% fiber volume fraction) were produced using a film-stacking procedure, the layers of ramie fabrics and PLA plate were piled up alternately as shown schematically in Figure 1. Layers of PLA plate and ramie fabric were compression molded with a conventional hot-press molding Toyoseiki Mini Test Press-10. The process condition for making composite panel was the same as process condition for making PLA plate. Figure 2 shows the materials and PLA/Ramie fabric laminate.

- **Tensile test**
  Fabrics. Ramie fabrics were tensile tested according to ASTM D 5035-11 on a Shimadzu Universal Tensile Tester, model AGS-10kNG. Fabric specimens prepared by the raveled strip method with the dimension of 50 mm x 150 mm. The fabrics were characterized in both warp and weft directions. Tensile tests were performed at a crosshead speed of 300 mm/minutes and a gauge length of 75 mm. Five specimens were tested to obtain average tensile properties.

  Polylactic acid (PLA). Tensile testing was carried out on a Shimadzu Universal Tensile Tester, model AGS-10kNG according to the ASTM D 638-14, with type IV specimen. Five specimens were tested with a crosshead speed of 5 mm/min and gauge length of 50 mm to obtain average tensile properties.

  Composite. Tensile properties of PLA/Ramie fabric laminates were characterized in accordance with ASTM D 3039/D 3039M-17. Tensile test was carried out using a Shimadzu Universal Tensile Tester, model AGS-10kNG. The machine was operated at a crosshead speed of 5 mm/min. Five specimens were tested to obtain average tensile properties composite.

- **Flexural test**
  Flexural test was conducted as per ASTM D 790-17. Specimens were loaded in three point bending with a recommended span to depth ratio of 16:1. The test was conducted on the same machine tensile test. Five specimens were tested and average result was obtained.

- **Impact test**
  The impact resistance of PLA/Ramie fabric composite in comparison to a pure PLA material was determined on unnotched izod test specimens in accordance with ASTM D 256-10 using CEAST Resil Impactor Junior. The tests were performed with energy pendulum of 2 Joule. A total of 5 samples of PLA and 5 of PLA/Ramie fabric composite were tested to determine mean impact resistance.

- **Scanning electron microscope**
  The specimens were coated with a thin layer of platinum (Pt) to get good conductivity, using Jeol Auto Fine Coater, model JFC-1600 apparatus before examination. The Ramie fiber and the fracture surfaces of tensile tests PLA/Ramie fabric specimens were observed by Jeol Analytical Scanning Electron Microscope (SEM), model JSM-6510LA.
RESULTS AND DISCUSSION

Tensile test
Ramie fabric tensile properties such as breaking force and percent apparent of elongation in both axial (0°-warp direction) and transverse (90°-weft direction) directions are summarized (Table 1). It was found that the breaking force in the axial and the transverse directions are different (Figure 3). Fracture type of ramie fabric at axial direction and test condition was shown (Figure 4). The plain woven ramie fabric has higher breaking force in the axial direction, as compared to the transverse direction. This occurs because the number of fibers at the same distance in the axial direction is more than the transverse direction. The tensile strength of rami fabric mostly 400-1000 MPa. In this case tensile strength of rami fabric 16.77 MPa at transverse direction and 22.94 MPa at axial direction. The duration and storage condition of sample might be causing it.

According to tensile test result of PLA and laminate composite, PLA has higher tensile strength compare to laminate at axial direction and transverse direction (Figure 5). Effect of reinforcement in laminate composite is not enough to improve PLA because tensile of ramie fabric lower than PLA as shown (Table 2). All specimens showed same type of fracture, brittle fracture as shown (Figure 6).

<table>
<thead>
<tr>
<th>Test direction</th>
<th>Maximum force (N)</th>
<th>Tensile strength (MPa)</th>
<th>Elongation at break (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Axial (0°-warp direction)</td>
<td>745.50 (66.08)</td>
<td>22.94 (2.03)</td>
<td>28.62 (5.14)</td>
</tr>
<tr>
<td>Transverse (90°-weft direction)</td>
<td>545.00 (61.06)</td>
<td>16.77 (1.88)</td>
<td>11.71 (3.76)</td>
</tr>
</tbody>
</table>

Note: Values in parentheses are standard deviations.

Figure 3. Typical Force-elongation diagram for ramie fabric in both axial, and transverse direction.

Figure 4. (a) Ramie fabric, (b) Tensile test for ramie fabric, (c) Tensile fracture specimen.

Figure 5. Typical tensile stress-elongation diagram for PLA and PLA/ramie fabric laminate.

Figure 6. Tensile, flexural, and izod impact resistance fractured laminate.
The results of flexural tests are shown in (Table 2). The average flexural strength of composite in both directions axial and transverse are 68.77 MPa and 91.11 MPa, respectively. An exception occurs where axial direction has a lower strength than transverse direction. It might be come from the preparation of specimens. PLA has a greater flexural modulus and flexural strength. Deterioration in flexural strength about 53% at axial direction and 37% at transverse direction to PLA occurred when ramie fabric is used to reinforce PLA. It caused by the low quality of ramie fiber as reinforcement like at tensile so it has a direct effect on the laminate composite. Composite laminate at axial direction has the longest displacement before break compare to PLA and laminate at transverse direction (Figure 7). During the test no specimen has failed by delamination and the failure mode shows no fiber pull-out.

**Table 2.** Mechanical properties of PLA, commercial synthetic resins and PLA/Ramie fabric laminate.

<table>
<thead>
<tr>
<th>Mechanical properties</th>
<th>PLA/Ramie fabric at axial direction</th>
<th>PLA/Ramie fabric at transverse direction</th>
<th>PLA</th>
<th>Epoxy</th>
<th>Polyester</th>
</tr>
</thead>
<tbody>
<tr>
<td>Tensile strength (MPa)</td>
<td>39.19 (1.55)</td>
<td>31.79 (1.30)</td>
<td>49.50 (5.34)</td>
<td>35-100</td>
<td>40-90</td>
</tr>
<tr>
<td>Tensile elongation (%)</td>
<td>2.32 (0.27)</td>
<td>1.38 (0.10)</td>
<td>2.03 (0.41)</td>
<td>1.0-6.0</td>
<td>2.0-5.0</td>
</tr>
<tr>
<td>Tensile modulus (GPa)</td>
<td>2.51 (0.10)</td>
<td>3.07 (0.14)</td>
<td>3.34 (0.13)</td>
<td>3.0-6.0</td>
<td>2.0-4.5</td>
</tr>
<tr>
<td>Flexural strength (MPa)</td>
<td>68.77 (11.43)</td>
<td>91.11 (7.64)</td>
<td>146.50 (11.69)</td>
<td>-</td>
<td>-</td>
</tr>
<tr>
<td>Flexural modulus (GPa)</td>
<td>3.22 (0.54)</td>
<td>3.67 (0.86)</td>
<td>4.38 (1.04)</td>
<td>-</td>
<td>-</td>
</tr>
<tr>
<td>Impact resistance (kJ/m²)</td>
<td>14.96 (2.13)</td>
<td>10.99 (2.52)</td>
<td>17.49 (3.25)</td>
<td>-</td>
<td>-</td>
</tr>
</tbody>
</table>

Note: Values in parentheses are standard deviations.

**Impact resistance test**

The results of unnotched Izod impact tests are shown in (Table 2). The average impact energy unit area of composite in both directions axial and transverse are 14.96 kJ/m² and 10.99 kJ/m², respectively. The two previous tests shown that PLA has the best performance compared to laminated composites because of the poor quality of ramie fabric. All specimen presented a complete break where the specimen separates into two pieces (Figure 6). In addition, the kinetic energy of the pendulum was transferred to the laminate during the contact, and consumed in the generation of damage. In terms of mechanical properties, the composite laminate still presented excellent energy absorption capabilities for engineering applications.

**Figure 8.** The SEM photograph of the PLA/Ramie fabric laminate tensile fracture. (a) Structure of laminate, (b) Matrix cracking.
**Scanning electron microscope**

Scanning electron microscope photographs of fractured surface of the composite after tensile test are shown in (Figure 8). As can be seen from (Figure 8-a), the composite was fabricated with one layer and it is possible to see different fabric and resin layer. At high magnification, the SEM photomicrograph of (Figure 8-b) show a matrix cracking at axial direction to the tensile loading and staggered brittle failure. It can also be seen in (Figure 9-a) the yarns in warp and weft directions, their fracture at different length and few cavities left by the pulled-out fibers.

![SEM images of composite fracture](image)

**Figure 9.** The SEM image showing a well bonded ramie fiber in the PLA matrix, (a) Fracture of yarn at different length, (b) Ramie fiber yarn, (c) Fiber bundles are attached to each other by the matrix, (d) Adhesion between the ramie fibers and the PLA matrix.

Furthermore, (Figure 9-b) shows SEM micrographs of single fibers. In contrast, (Figure 9-c) show that the fiber bundles are attached to each other by the matrix, which indicates that the PLA penetrates the yarn. Additionally, Figure 9(d) exhibit that ramie fibers are well bonded to PLA matrix, gaps in the fiber and polymer interface are not found and the PLA matrix and the fiber surfaces are not clean, which indicates good adhesion between the ramie fibers and the PLA matrix.

**Discussion**

In this work, Ramie fabric and 3D printed PLA filament were used to fabricate fully biodegradable laminate, an attractive combination of mechanical properties with their environmental friendly character. According to tensile test of fabric, the warp direction has higher breaking force compared to the weft direction. In reference to the characterization of the laminate composite, laminate with warp direction higher than weft direction. Also scanning electron microscopy analysis showed good bonding between Ramie fiber and PLA matrix.

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